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REPORT NO. RS-TR-70-6

# RAPID HEATING AND LOADING OF 7675 - T6 ALUMINUM ALLOY SHEET

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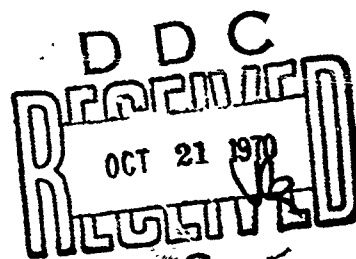
John H. Honeycutt

May 1970

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Report No. RS-TR-70-6

## **RAPID HEATING AND LOADING OF 7075 - T6 ALUMINUM ALLOY SHEET**

by

**John H. Honeycutt**

**DA Project No. IT062105A328  
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**Materials Engineering and Development Branch  
Structures and Mechanics Laboratory  
Research and Engineering Directorate  
U. S. Army Missile Command  
Redstone Arsenal, Alabama 35809**

### **Abstract**

The purpose of this report is to make available to the design engineer tensile property data on 7075-T6 aluminum, in the longitudinal and transverse directions, under conditions of rapid heating and loading.

The tensile property data reported are: ultimate tensile stress, ultimate yield stress (at 0.2-percent offset), elastic modulus, percent total elongation, and percent uniform elongation. These tensile properties were determined at strain rates of 0.0047, 0.0201, and 0.0266 in./in./sec and at temperatures from room temperature (78°F) to 700°F at 100° intervals, excluding 100° and 200°F. The time required to reach test temperature was, in most cases, less than 10 seconds.

Primary consideration is given to ultimate tensile and yield properties. Other tensile property data reported are secondary and should be used for design criteria only after consideration has been given to the methods used for obtaining and reducing these data.

The strength properties of the test material increased with an increase in strain rate from 300° to 700°F with one exception at 500°F on the transverse specimens. However, from room temperature to 300°F, the strength properties showed almost no change with respect to strain rate except for a point at room temperature on the longitudinal specimens.

### **Acknowledgement**

The efforts of Malcolm Bumbalough in assembling the apparatus and modifying the electronics to provide accurate data and of Keith Bates in aiding in the reduction of data are gratefully acknowledged.

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## 1. Introduction

Four aluminum alloys were selected for tensile property evaluation at various strain rates and temperatures; they are 2014-0, 2024-T3, 7075-T6, and 5052-H34. At this time, only the 5052-H34 and the 7075-T6 alloys have been evaluated.<sup>1</sup>

The controlling factor for the strain rates to be used is the test equipment now on hand. These strain rates are 0.0047, 0.0201, and 0.0266 in./in./sec. The strain rates are not constant and are an average of the strain rates for each test condition.

The temperature for this investigation ranged from room temperature (78°F) to 700°F at 100° intervals, excluding 100° and 200°F. The test samples were resistance heated and the temperature was manually controlled by visually monitoring a thermocouple output. The time required to reach test temperature was approximately 10 seconds for all specimens.

To record the test, an X-Y recorder was employed at the slower strain rate (0.0047 in./in./sec). At the other two strain rates (0.0201 and 0.0266 in./in./sec), an oscilloscope with a Polaroid camera was used to record the test data. The reason for the instrumentation change was that the X-Y recorder slew rate is 20 in./sec and the loading rate of the specimens at the two faster strain rates is greater than 20 in./sec, which is too fast for the recorder.

Two specimens were required to establish a data point, if the data agreed within 10 percent. If the data did not agree within 10 percent, a third specimen was tested. The data used to plot the curves were averages of either two or three data points recorded.

Testing of the two other alloys is being held in abeyance until new test equipment is installed. This new equipment will provide a controlled strain and an increase in the strain differential.

## 2. Test Material

The 7075-T6 material used for this test was a sheet measuring 36 by 36 inches, 0.50 inch thick, which was furnished by the Reynolds Metals

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<sup>1</sup>Honeycutt, J. H., Rapid Heating and Loading of 5052-H34 Aluminum Alloy Sheet, U. S. Army Missile Command, Redstone Arsenal, Alabama, Report No. RS-TR-69-2.



Company. No chemical composition was furnished. The test specimen configuration is shown in Figure 1.

### 3. Test Equipment

The test equipment used for tensile loading of the specimens was a Model TTD Instron universal testing machine with a full scale load capability of 20,000 pounds. Specimens were resistance-heated by use of a Marquardt TM9 power controller.

The recorder instrument used for the slower strain rate (0.0047 in./in./sec) was a Model 2D Mosley X-Y recorder. A Tektronix Model 502A dual-beam oscilloscope with Polaroid camera attached was used to record data at the two faster strain rates (0.0201 and 0.0266 in./in./sec).

The temperature of the specimen was controlled manually during observation of the temperature recorder. The temperature recorder monitored a chromel-alumel thermocouple, which was attached to the center of the gage length of the specimen by percussive welding.

The specimen strain was measured with a clip-on type extensometer over the 2-inch gage length of the specimen (Figure 2).

A block diagram of the test setup and associated instrumentation is shown in Figure 3.

### 4. Data Measurement

The specimen load was measured with an Instron load cell. This is an electronically calibrated strain-gage type cell with load ranges of 500, 1000, 2000, 5000, 10,000, and 20,000 pounds.

Strain measurements were made with the clip-on type extensometer. This extensometer consists of a 0.5-inch wide by 3-inch long piece of spring steel with appropriate clamps fastened to each end (Figure 2). There are two strain gages mounted on both the tension and compression side of the spring. The extensometer bridge network and physical arrangement of the gages are shown in Figure 4. This bridge arrangement is such that strain signals in  $R_1$  and  $R_3$  are additive in one direction and those of  $R_2$  and  $R_4$  are additive in the other direction, thus producing four times the electrical output of a single strain gage.

The strain rate for each test condition was measured with the second beam on the oscilloscope indicating strain only. A pulse generator caused the second beam to be displayed on the oscilloscope at a predetermined time interval of 15, 30, 60, or 100 milliseconds.

The strain rate beam sweep is shown in the upper part of Figure 5.

The strain rate reported for each condition was calculated from the load-strain curves at that condition. The strain rate was calculated over the portion of the curve from zero strain to the 0.2-percent offset yield point and is the average strain rate for each individual test sample (Figure 5).

In all cases the strain rate showed a definite increase after the specimen reached its proportional limit. This increase was a result of some of the cross-head movement being taken up by the elastic deformation of the test machine parts such as the load cell, pull rods, jaws, universal joints, and specimen shoulders.

Temperature measurements were read directly from a temperature meter, which is calibrated in degrees Fahrenheit. The meter was driven by a chromel-alumel thermocouple welded to the center of the gage length of the specimen. The temperature was manually controlled because of the slow response to temperature change of the automatic temperature controller.

The percent total elongation of each specimen was measured by use of a Riehle percent gage for a 2-inch gage length. In some instances, the specimens that were run at other than room temperature arched upon fracture, causing the ends of the fractured part of the specimen to melt (Figure 6). Because of the arcing and consequent melting of the material, it was not possible to measure the percent total elongation with a consistent degree of accuracy.

The uniform elongation measurements were taken from the recorded data of the calibrated extensometer. Figure 7 shows a typical curve from which the uniform elongation was calculated.

The angle of fracture of each specimen was measured with an adjustable protractor. A fracture perpendicular to the load axis was considered a fracture angle of 0 degree.

## 5. Test Procedure

Specimens oriented in both the longitudinal and transverse directions were evaluated. The longitudinal specimens were tested first. The test was

started at the slower strain rate (0.0047 in./in./sec) and at each strain rate specimens were tested at 700°, 600°, 500°, 400°, and 300°F, and at room temperature. At each temperature, only two specimens were tested if the tensile data agreed within 10 percent. If the tensile data did not agree within 10 percent, a third specimen was tested. The average tensile data from the two or three specimens were then used as the data point to construct all curves.

At the beginning of each test, all specimens were marked and measured, and their areas calculated and recorded.

Before the beginning of each test period, a sample specimen was mounted in the test machine and the temperature gradients were checked. When necessary, adjustments were made to keep the temperature gradients within 10°F or less over the gage length of the specimen. Periodic checks were made as required during the test period to maintain this minimum temperature gradient (Figure 8).

A specimen was clamped in the machine and a thermocouple percussively welded to the center of its gage length. The thermocouple was used to control and measure the temperature of the specimen. Next, the calibrated extensometer was clipped on the specimen and the specimen brought up to the desired temperature within 10 seconds or less. At this time, the load was applied to the specimen and the load-strain curve was recorded on the oscilloscope for the two faster strain rates (0.0266 and 0.0201 in./in./sec) and on the Mosley X-Y recorder at the slower strain rate (0.0047 in./in./sec).

During the test, the temperature was manually controlled by observation of the temperature meter. Manual control of the specimen temperature was held within  $\pm 10^\circ\text{F}$  throughout the specimen test cycle.

The ultimate strength and 0.2-percent offset yield were determined from each calibrated load-strain curve. Modulus of elasticity was measured from the slope of the elastic portion of the load-strain curves (Figure 5). Total elongation was measured by use of a Riehle percent gage and the angle of fracture was measured with a protractor.

The strain rate for each test was calculated from the timing information on the oscilloscope trace as recorded on the load-strain curve (upper trace on the load-strain curve, Figure 5). As shown in this figure, the strain rate is 0.026 in./in./sec from zero strain to the 0.2-percent offset yield load on the strain axis. From this point, 2 centimeters out on the strain axis, the strain rate increases to 0.046 in./in./sec. The reasons for the lower strain rate are

that pull rods, universal joints, load cell, and specimen shoulders have some elastic deformation that takes up some of the movement of the crosshead, which travels at a constant rate. The strain rates reported here are average rates taken from the start of loading to the 0.2-percent offset yield strength.

In each test for uniform elongation, the extensometer was left on the sample until failure. From the data plotted on the X-Y recorder, the uniform elongation was calculated by use of the recorded values of strain from the calibrated extensometer (Figure 7).

## 6. Test Results

The results of these tests are shown in Tables I through VI. The curves representing the average tabulated values are shown in Figures 9 through 24. The data points of each curve are an average of either two or three specimens as shown in the tabulated data.

### a. Ultimate Tensile Properties

Ultimate tensile properties decrease moderately with an increase in temperature up to 300°F. However, past 300°F, the strength properties decrease sharply to 700°F.

The strain rates appear to have almost no effect on the stress values. This is particularly true for the transverse curves from room temperature to 300°F for all strain rates. Also the 0.0201-in./in./sec strain rate is erratic and shows stress levels different from the 0.0266 strain rate only between 500° and 700°F.

The general trend for both the longitudinal and transverse directions is approximately the same.

### b. Yield Properties (at 0.2-Percent Offset)

The 0.2-percent offset yield curves for both longitudinal and transverse data show approximately the same trends as the ultimate tensile curve. However, the 0.0201-in./in./sec longitudinal curve shows a stress value below that of the ultimate curve at room temperature. This is probably due to the construction of the modulus line for this particular point. This low point represents an error of approximately 8 percent.

c. Elastic Modulus

The elastic modulus curves show a decrease in modulus with an increase in temperature up to 500°F, above which the modulus increases with an increase in temperature. However, the 0.0201- and 0.0047-in./in./sec longitudinal curves show a decreasing modulus value from room temperature to 700°F.

At the faster strain rate, the transverse and longitudinal specimens have comparable modulus values at corresponding temperatures. The intermediate strain rate of the longitudinal specimens as compared to the transverse specimens show higher modulus values at room temperature and 200°F; lower modulus values at 500°, 600°, and 700°F; and at 300° and 400°F, the modulus values are the same. At the slower strain rate, the longitudinal and transverse specimens exhibit approximately the same modulus values at corresponding temperatures, except at 700°F. At 700°F, the transverse specimen shows an increase in modulus of 56 percent compared to the longitudinal specimen.

d. Total Elongation

Both the longitudinal and transverse total elongation curves show the same trends with respect to temperature. That is, there is little change in elongation from room temperature to 550°F. However, from 550° to 700°F, there is a pronounced increase in total elongation for both longitudinal and transverse curves at all strain rates.

The average increase in total elongation in this temperature range is 213 and 150 percent for the longitudinal and transverse specimens, respectively.

e. Uniform Elongation

Uniform elongation is considered to be the elongation of the specimen that occurs before any decrease in load is observed on the recorded data. It is therefore the usable elongation in design. The trend of uniform elongation in relation to temperature is just the reverse of that exhibited by total elongation, decreasing with increasing temperature. In the design of missiles, this type of data can be extremely important where low factors of safety inherent in "one-shot" hardware are used.

The longitudinal and transverse curves are erratic at all strain rates. However, the longitudinal and transverse curves of the intermediate strain rate of 0.0201 in./in./sec show more uniformity than the curves of the other two strain rates of 0.0266 and 0.0047 in./in./sec.

f. Angle of Fracture

The angle of fracture for this material was 0 degrees in most cases. Only on two occasions was the average angle of fracture value over 5 degrees. These values were 6.5 degrees at 300° F and 6 degrees at 600° F for the longitudinal and transverse specimens, respectively, at a strain rate of 0.0266 in./in./sec.

No effort has been made to analyze the angle of fracture data by crystallographic or other means; they are reported simply as a matter of interest.

g. Stress-Strain

The stress-strain curves for all strain rates show decrease in stress with increasing temperature. The effect of increased strain rate shows an increase in stress level at corresponding temperatures for both the longitudinal and transverse specimens.

7. Conclusions

All properties evaluated in this test followed previously established trends with respect to temperature and strain rate. The trend established for uniform elongation shows a decrease in elongation with an increase in temperature.

Strain rates used for test conditions were not differentiated sufficiently to establish unquestionable trends with respect to strain rates in most cases. The ultimate yield and total elongation longitudinal curves are examples of this condition.

For design of missiles, the uniform elongation may be of significant importance and considerably more quantitative data concerning this parameter should be generated before they are used as design criteria.

TABLE I. TENSILE PROPERTIES OF 7075-T6 ALUMINUM SHEET (LONGITUDINAL SPECIMEN, 20 in./min)

| Spec No.            | Spec Area | Temp (°F) | Strain Rate (in./in./sec) | Ult Load (lb) | Ult Stress (psi) | Yield, 2-Percent Offset (lb) | Yield Stress (psi) | Elastic Modulus ( $\times 10^6$ psi) | Elong, Total (%) | Elong, Uniform (%) | Angle of Fracture (deg) |
|---------------------|-----------|-----------|---------------------------|---------------|------------------|------------------------------|--------------------|--------------------------------------|------------------|--------------------|-------------------------|
| 1                   | 0.0260    | 700       | 0.0258                    | 334           | 12,846           | 309                          | 11,885             | 21.4                                 | 25.0             | 3.3                | 0                       |
| 2                   | 0.0255    | 700       | 0.0258                    | 304           | 11,919           | 287                          | 11,264             | 21.0                                 | 31.0             | 3.0                | 0                       |
| Av                  |           |           | 0.0258                    | 319           | 12,383           | 298                          | 11,575             | 21.2                                 | 28.0             | 3.2                | 0                       |
| 4*                  | 0.0237    | 600       | 0.0250                    | 518           | 20,744           | 501                          | 19,494             | 15.5                                 | 11.0             | 3.2                | 0                       |
| 5                   | 0.0262    | 600       | 0.0283                    | 523           | 19,955           | 503                          | 19,192             | 15.2                                 | 12.0             | 3.2                | 0                       |
| Av                  |           |           | 0.0267                    | 521           | 20,050           | 502                          | 19,343             | 15.4                                 | 11.5             | 3.2                | 0                       |
| 6                   | 0.0256    | 500       | 0.0250                    | 895           | 34,960           | 872                          | 34,023             | 15.2                                 | 6.0              | 2.9                | 0                       |
| 7                   | 0.0256    | 500       | 0.0266                    | 835           | 32,617           | 812                          | 31,704             | 15.5                                 | 7.0              | 2.8                | 0                       |
| Av                  |           |           | 0.0258                    | 865           | 33,789           | 842                          | 32,864             | 15.4                                 | 6.5              | 2.8                | 0                       |
| 8                   | 0.0256    | 400       | 0.0275                    | 1327          | 51,849           | 1281                         | 50,250             | 15.5                                 | 10.0             | 6.0                | 5.0                     |
| 9                   | 0.0256    | 400       | 0.0308                    | 1300          | 50,807           | 1281                         | 48,462             | 15.5                                 | 10.0             | 5.0                | 0                       |
| Av                  |           |           | 0.0292                    | 1314          | 51,328           | 1281                         | 49,356             | 15.5                                 | 10.0             | 5.5                | 2.5                     |
| 10                  | 0.0255    | 300       | 0.0241                    | 1740          | 68,269           | 1641                         | 64,346             | 14.7                                 | 11.0             | 7.0                | 7.0                     |
| 11                  | 0.0255    | 300       | 0.0283                    | 1748          | 68,331           | 1654                         | 64,869             | 14.2                                 | 10.0             | 7.0                | 6.0                     |
| Av                  |           |           | 0.0262                    | 1744          | 68,300           | 1648                         | 64,608             | 14.5                                 | 10.5             | 7.0                | 6.5                     |
| 12                  | 0.0255    | RT        | 0.0275                    | 2025          | 79,412           | 1845                         | 72,346             | 15.0                                 | 11.0             | 10.0               | 0                       |
| 13                  | 0.0258    | RT        | 0.0266                    | 2010          | 81,436           | 1914                         | 74,197             | 15.4                                 | 11.0             | 10.0               | 7.0                     |
| Av                  |           |           | 0.0271                    | 2018          | 80,424           | 1880                         | 73,272             | 15.2                                 | 11.0             | 10.0               | 3.5                     |
| Average strain rate |           |           | 0.0268                    |               |                  |                              |                    |                                      |                  |                    |                         |

\* Specimen No. 3 omitted. Expansion control failed to work properly.

TABLE II. TENSILE PROPERTIES OF 7075-T6 ALUMINUM SHEET (TRANSVERSE SPECIMEN, 20 in./min)

| Spec No.            | Spec Area | Temp (°F) | Strain rate (in./in./sec) | Ult Load (lb) | Ult Stress (psi) | Yield, 2-Percent Offset (lb) | Yield Stress (psi) | Elastic Modulus ( $\times 10^6$ psi) | Elong, Total (%) | Elong, Uniform (%) | Angle of Fracture (deg) |
|---------------------|-----------|-----------|---------------------------|---------------|------------------|------------------------------|--------------------|--------------------------------------|------------------|--------------------|-------------------------|
| 1                   | 0.0257    | 700       | 0.0267                    | 364           | 14,163           | 339                          | 13,191             | 20.3                                 | 28.0             | 3.6                | 5.0                     |
| 2                   | 0.0256    | 700       | 0.0225                    | 359           | 14,025           | 342                          | 13,373             | 21.7                                 | 29.0             | 3.2                | 0.0                     |
| Av                  |           |           | 0.0246                    | 362           | 14,106           | 340                          | 13,282             | 21.0                                 | 28.5             | 3.4                | 2.5                     |
| 3                   | 0.0256    | 600       | 0.0208                    | 576           | 22,506           | 546                          | 21,364             | 18.1                                 | 12.0             | 2.9                | 5.0                     |
| 4                   | 0.0256    | 600       | 0.0267                    | 569           | 22,226           | 538                          | 21,000             | 18.1                                 | 12.0             | 3.0                | 7.0                     |
| Av                  |           |           | 0.0238                    | 572           | 22,366           | 542                          | 21,182             | 18.1                                 | 12.0             | 2.95               | 6.0                     |
| 5                   | 0.0256    | 500       | 0.0300                    | 912           | 35,641           | 882                          | 34,470             | 12.3                                 | 11.0             | 3.6                | 7.0                     |
| 6                   | 0.0256    | 500       | 0.0267                    | 989           | 38,633           | 942                          | 36,812             | 13.5                                 | 10.0             | 3.6                | 0.0                     |
| Av                  |           |           | 0.0283                    | 950           | 37,137           | 912                          | 35,641             | 12.9                                 | 10.5             | 3.6                | 3.5                     |
| 7                   | 0.0255    | 400       | 0.0267                    | 1315          | 51,582           | 1225                         | 48,056             | 15.2                                 | 9.0              | 4.40               | 0                       |
| 8                   | 0.0255    | 400       | 0.0250                    | 1385          | 54,325           | 1315                         | 51,582             | 14.2                                 | 8.0              | 3.70               | 0                       |
| Av                  |           |           | 0.0258                    | 1350          | 52,954           | 1270                         | 49,819             | 14.7                                 | 8.5              | 4.05               | 0                       |
| 9                   | 0.0255    | 300       | 0.0292                    | 1814          | 71,146           | 1661                         | 65,131             | 13.5                                 | 10.0             | 7.60               | 0                       |
| 10                  | 0.0255    | 300       | 0.0292                    | 1781          | 69,839           | 1628                         | 63,823             | 13.8                                 | 10.0             | 7.20               | 0                       |
| Av                  |           |           | 0.0292                    | 1798          | 70,492           | 1642                         | 64,477             | 13.65                                | 10.0             | 7.40               | 0                       |
| 11                  | 0.0255    | RT        | 0.0267                    | 2081          | 81,609           | 1801                         | 70,623             | 15.6                                 | 11.0             | 10.20              | 0                       |
| 12                  | 0.0255    | RT        | 0.0267                    | 2058          | 81,871           | 1814                         | 71,141             | 16.0                                 | 11.0             | 10.20              | 0                       |
| Av                  |           |           | 0.0267                    | 2084          | 81,740           | 1808                         | 70,882             | 15.8                                 | 11.0             | 10.20              | 0                       |
| Average strain rate |           |           | 0.0264                    |               |                  |                              |                    |                                      |                  |                    |                         |



TABLE III. TENSILE PROPERTIES OF 7075-T6 ALUMINUM SHEET (LONGITUDINAL SPECIMEN, 10 in./min)

| Spec No.            | Spec Area | Temp (°F) | Strain Rate (in./in./sec) | Ult Load (lb) | Ult Stress (psi) | Yield, 2-Percent Offset (lb) | Yield Stress (psi) | Elastic Modulus ( $\times 10^6$ psi) | Elong, Total (%) | Elong, Uniform (%) | Angle of Fracture (deg) |
|---------------------|-----------|-----------|---------------------------|---------------|------------------|------------------------------|--------------------|--------------------------------------|------------------|--------------------|-------------------------|
| 1                   | 0.0263    | 700       | 0.0250                    | 270           | 10,266           | 270                          | 10,266             | 8.6                                  | 23.0             | 0.5                | 0                       |
| 2                   | 0.0262    | 700       | 0.0200                    | 270           | 10,305           | 270                          | 10,305             | 9.9                                  | 22.0             | 0.5                | 0                       |
| Av                  |           |           | 0.0225                    | 270           | 10,286           | 270                          | 10,286             | 9.3                                  | 22.5             | 0.5                | 0                       |
| 4                   | 0.0262    | 600       | 0.0241                    | 446           | 17,022           | 446                          | 17,022             | 10.4                                 | 12.0             | 0.5                | 0                       |
| 5                   | 0.0262    | 600       | 0.0175                    | 424           | 16,183           | 424                          | 16,183             | 10.5                                 | 12.0             | 0.6                | 0                       |
| Av                  |           |           | 0.0208                    | 435           | 16,603           | 435                          | 16,603             | 10.45                                | 12.0             | 0.55               | 0                       |
| 6                   | 0.0262    | 500       | 0.0166                    | 836           | 32,154           | 824                          | 31,692             | 9.7                                  | 8.0              | 1.0                | 0                       |
| 7                   | 0.0260    | 500       | 0.0158                    | 826           | 31,783           | 808                          | 30,149             | 10.0                                 | 8.0              | 1.0                | 0                       |
| Av                  |           |           | 0.0162                    | 828           | 31,969           | 816                          | 30,921             | 9.9                                  | 8.0              | 1.0                | 0                       |
| 8                   | 0.0258    | 400       | 0.0208                    | 1288          | 49,349           | 1216                         | 46,590             | 12.8                                 | 8.0              | 1.0                | 0                       |
| 9                   | 0.0261    | 400       | 0.0241                    | 1229          | 47,636           | 1156                         | 44,806             | 11.8                                 | 9.0              | 3.0                | 0                       |
| Av                  |           |           | 0.0225                    | 1259          | 48,493           | 1186                         | 45,698             | 12.3                                 | 8.5              | 2.0                | 0                       |
| 10                  | 0.0258    | 300       | 0.0216                    | 1744          | 67,597           | 1640                         | 63,566             | 13.6                                 | 9.0              | 2.0                | 0                       |
| 11                  | 0.0259    | 300       | 0.0225                    | 1744          | 67,335           | 1643                         | 63,436             | 12.8                                 | 10.0             | 2.0                | 0                       |
| Av                  |           |           | 0.0221                    | 1744          | 67,466           | 1642                         | 63,501             | 13.2                                 | 9.5              | 2.0                | 0                       |
| 12                  | 0.0255    | RT        | 0.0208                    | 2197          | 86,157           | 1761                         | 69,059             | 16.2                                 | 12.0             | 10.0               | 0                       |
| 13                  | 0.0255    | RT        | 0.0200                    | 2235          | 85,632           | 1734                         | 66,460             | 16.7                                 | 11.0             | 10.0               | 0                       |
| Av                  |           |           | 0.0204                    | 2216          | 85,895           | 1748                         | 67,760             | 16.3                                 | 11.5             | 10.0               | 0                       |
| Average strain rate |           |           | 0.0208                    |               |                  |                              |                    |                                      |                  |                    |                         |

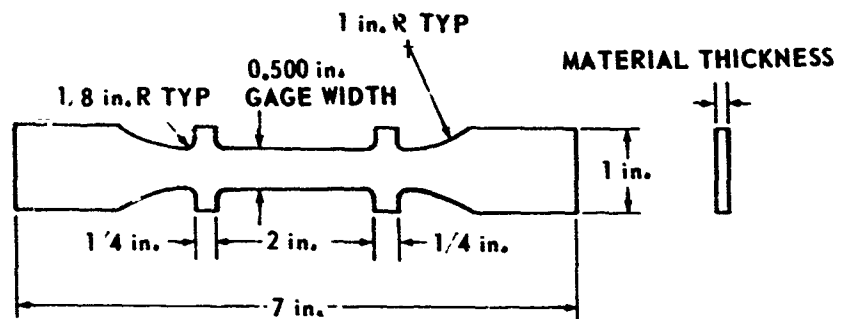
TABLE IV. TENSILE PROPERTIES OF 7075-T6 ALUMINUM SHEET (TRANSVERSE SPECIMEN, 10 in./min)

| Spec No.            | Spec Area | Temp (°F) | Strain Rate (in./in./sec) | Ult Load (lb) | Ult Stress (psi) | Yield, 2-Percent Offset (lb) | Yield Stress (psi) | Elastic Modulus ( $\times 10^6$ psi) | Elong, Total (%) | Elong, Uniform (%) | Angle of Fracture (deg) |
|---------------------|-----------|-----------|---------------------------|---------------|------------------|------------------------------|--------------------|--------------------------------------|------------------|--------------------|-------------------------|
| 1                   | 0.0257    | 700       | 0.0183                    | 306           | 11,907           | 306                          | 11,907             | 20.3                                 | 28.0             | 0.83               | 0                       |
| 2                   | 0.0256    | 700       | 0.0217                    | 306           | 11,971           | 306                          | 11,971             | 13.0                                 | 30.0             | 0.76               | 5.0                     |
| Av                  |           |           | 0.0200                    | 306           | 11,939           | 306                          | 11,939             | 16.65                                | 29.0             | 0.80               | 2.5                     |
| 3                   | 0.0256    | 600       | 0.0208                    | 496           | 19,375           | 481                          | 18,788             | 17.2                                 | 14.0             | 0.46               | 0                       |
| 4                   | 0.0256    | 600       | 0.0192                    | 524           | 20,484           | 509                          | 19,896             | 16.3                                 | 14.0             | 0.46               | 0                       |
| Av                  |           |           | 0.0200                    | 510           | 19,930           | 495                          | 19,342             | 16.75                                | 14.0             | 0.46               | 0                       |
| 5                   | 0.0256    | 500       | 0.0200                    | 992           | 38,763           | 956                          | 37,332             | 12.5                                 | 8.0              | 1.8                | 5.0                     |
| 6                   | 0.0256    | 500       | 0.0200                    | 1046          | 40,845           | 966                          | 37,723             | 13.0                                 | 12.0             | 2.2                | 0                       |
| Av                  |           |           | 0.0200                    | 1019          | 39,804           | 961                          | 37,527             | 12.75                                | 10.0             | 2.0                | 2.5                     |
| 7                   | 0.0256    | 400       | 0.0192                    | 1327          | 51,849           | 1217                         | 47,550             | 12.9                                 | 10.0             | 4.8                | 0                       |
| 8                   | 0.0256    | 400       | 0.0200                    | 1354          | 52,891           | 1234                         | 48,201             | 12.8                                 | 11.0             | 4.8                | 6.0                     |
| Av                  |           |           | 0.0196                    | 1340          | 52,370           | 1226                         | 47,876             | 12.85                                | 10.5             | 4.8                | 3.0                     |
| 9                   | 0.0256    | 300       | 0.0192                    | 1774          | 69,305           | 1557                         | 60,838             | 12.6                                 | 11.0             | 7.2                | 0                       |
| 10                  | 0.0254    | 300       | 0.0175                    | 1781          | 70,114           | 1567                         | 61,711             | 12.6                                 | 13.0             | 8.4                | 0                       |
| Av                  |           |           | 0.0183                    | 1778          | 69,710           | 1562                         | 61,274             | 12.6                                 | 12.0             | 7.8                | 0                       |
| 11                  | 0.0255    | RT        | 0.0183                    | 2041          | 80,040           | 1754                         | 68,793             | 13.7                                 | 11.0             | 10.1               | 0                       |
| 12                  | 0.0256    | RT        | 0.0175                    | 2081          | 81,289           | 1768                         | 69,045             | 13.1                                 | 11.0             | 10.2               | 0                       |
| Av                  |           |           | 0.0178                    | 2061          | 80,664           | 1761                         | 68,919             | 13.4                                 | 11.0             | 10.15              | 0                       |
| Average strain rate |           |           | 0.0193                    |               |                  |                              |                    |                                      |                  |                    |                         |

[illegible]

TABLE VI. TENSILE PROPERTIES OF 7075-T6 ALUMINUM SHEET (TRANSVERSE SPECIMEN, 1 in./min)

| Spec No.            | Spec Area | Temp (°F) | Strain Rate (in./in./sec) | Ult Load (lb) | Ult Stress (psi) | Yield, 2-Percent Offset (lb) | Yield Stress (psi) | Elastic Modulus ( $\times 10^6$ psi) | Elong, Total (%) | Elong, Uniform (%) | Angle of Fracture (deg) |
|---------------------|-----------|-----------|---------------------------|---------------|------------------|------------------------------|--------------------|--------------------------------------|------------------|--------------------|-------------------------|
| 1                   | 0.0258    | 700       | 0.00483                   | 233           | 9031             | 233                          | 9031               | 8.2                                  | 28.0             | 0.40               | 0                       |
| 2                   | 0.0259    | 700       | 0.00475                   | 230           | 8891             | 230                          | 8891               | 8.2                                  | 31.0             | 0.34               | 0                       |
| Av                  |           |           | 0.00479                   | 232           | 8961             | 232                          | 8961               | 8.2                                  | 29.5             | 0.37               | 0                       |
| 3                   | 0.0256    | 600       | 0.00383                   | 429           | 16,758           | 427                          | 16,680             | 6.3                                  | 14.0             | 0.74               | 0                       |
| 4                   | 0.0256    | 600       | 0.00617                   | 437           | 16,928           | 406                          | 15,728             | 6.2                                  | 18.0             | 0.62               | 0                       |
| Av                  |           |           | 0.00500                   | 433           | 16,843           | 416                          | 16,204             | 6.15                                 | 16.0             | 0.78               | 0                       |
| 5                   | 0.0256    | 500       | 0.00533                   | 826           | 32,266           | 802                          | 31,328             | 6.5                                  | 9.5              | 2.6                | 0                       |
| 6                   | 0.0256    | 500       | 0.00517                   | 802           | 32,672           | 838                          | 32,734             | 6.9                                  | 9.5              | 2.5                | 0                       |
| Av                  |           |           | 0.00525                   | 839           | 32,969           | 820                          | 32,031             | 6.7                                  | 9.5              | 2.55               | 0                       |
| 7                   | 0.0255    | 400       | 0.00467                   | 1250          | 49,020           | 1170                         | 45,882             | 7.8                                  | 13.0             | 6.6                | 0                       |
| 8                   | 0.0255    | 100       | 0.00458                   | 1260          | 49,412           | 1198                         | 46,980             | 8.2                                  | 13.0             | 4.5                | 0                       |
| Av                  |           |           | 0.00462                   | 1255          | 49,216           | 1184                         | 46,431             | 8.0                                  | 13.0             | 5.55               | 0                       |
| 9                   | 0.0255    | 300       | 0.00383                   | 1714          | 68,392           | 1616                         | 63,373             | 8.9                                  | 12.0             | 6.7                | 0                       |
| 10                  | 0.0255    | 300       | 0.00383                   | 1688          | 66,196           | 1576                         | 61,804             | 8.7                                  | 12.0             | 6.9                | 0                       |
| Av                  |           |           | 0.00383                   | 1716          | 67,294           | 1596                         | 62,588             | 8.8                                  | 12.0             | 6.8                | 0                       |
| 11                  | 0.0258    | RT        | 0.00517                   | 2120          | 82,171           | 1896                         | 73,488             | 9.5                                  | 11.5             | 10.2               | 0                       |
| 12                  | 0.0258    | RT        | 0.00492                   | 2112          | 81,860           | 1872                         | 72,588             | 9.5                                  | 11.5             | 10.4               | 0                       |
| Av                  |           |           | 0.00504                   | 2116          | 82,056           | 1884                         | 73,023             | 9.5                                  | 11.5             | 10.3               | 0                       |
| Average strain rate |           |           | 0.00476                   |               |                  |                              |                    |                                      |                  |                    |                         |



The thickness of machined specimens within the reduced section shall be uniform within 0.010 inch.

The ends of reduced section shall not differ in width by more than 0.002 inch. There may be a gradual taper in width from the ends to the center, but the width at either end shall not be more than 0.005 inch greater than the width at the center.

FIGURE 1. DIAGRAM OF TENSILE SPECIMEN



FIGURE 2. CLIP-ON EXTENSOMETER AND TEST SPECIMEN

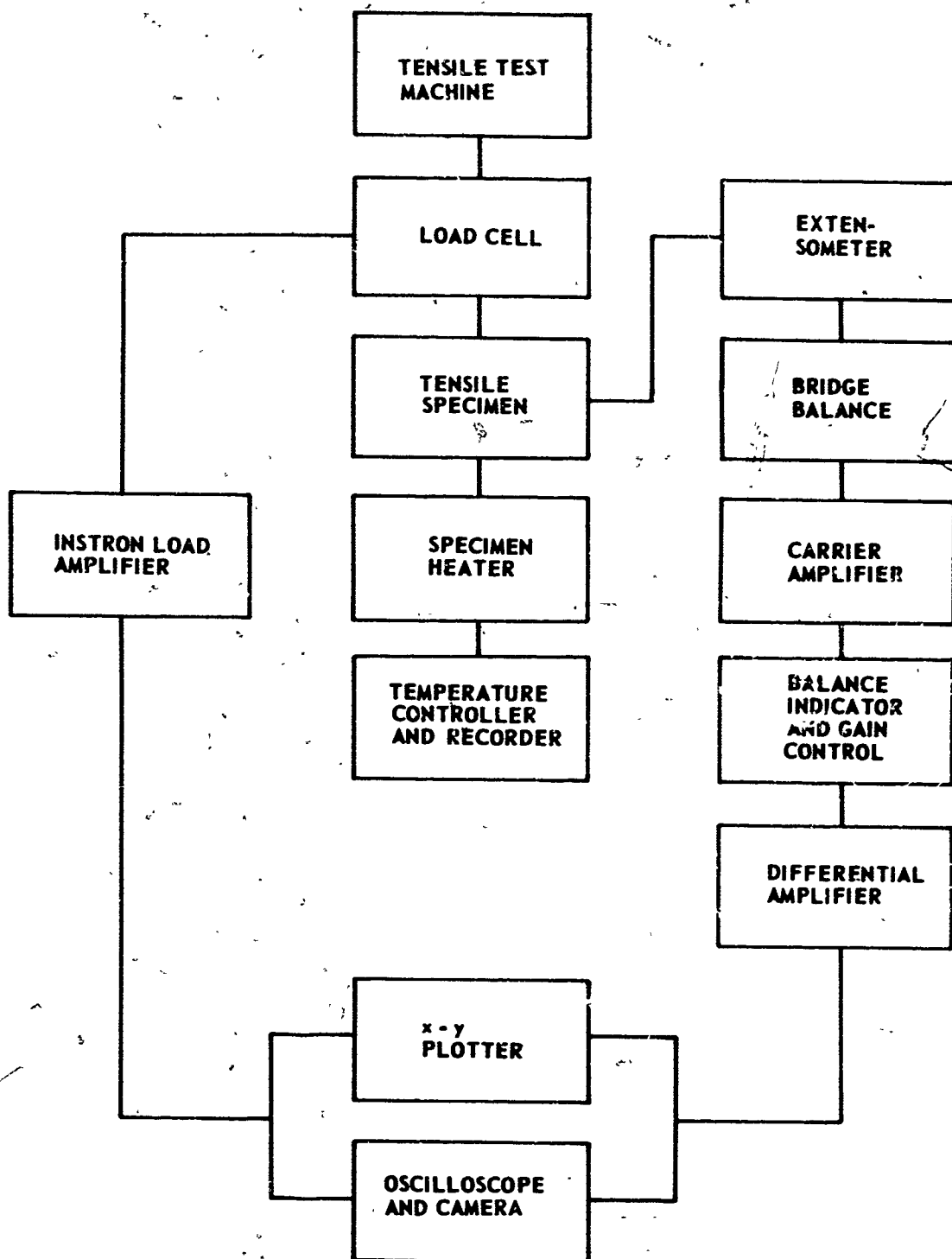


FIGURE 3. FUNCTIONAL DIAGRAM OF TEST SETUP

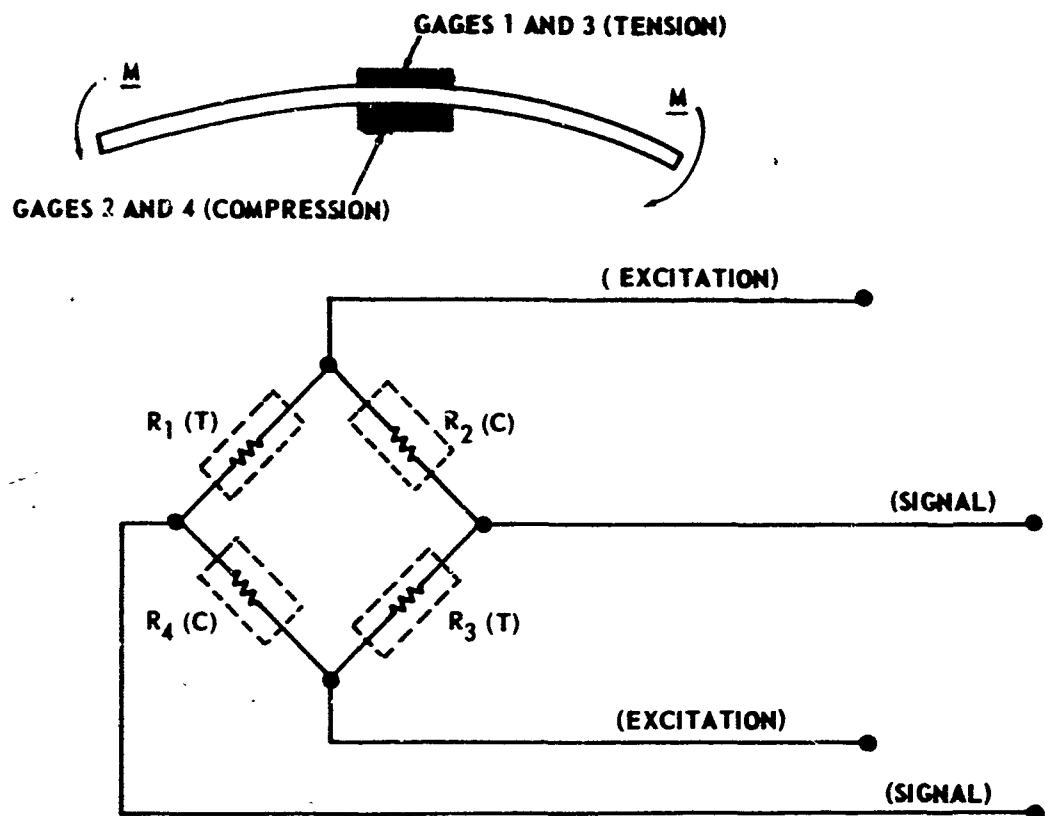


FIGURE 4. EXTENSOMETER PHYSICAL ARRANGEMENT AND BRIDGE NETWORK

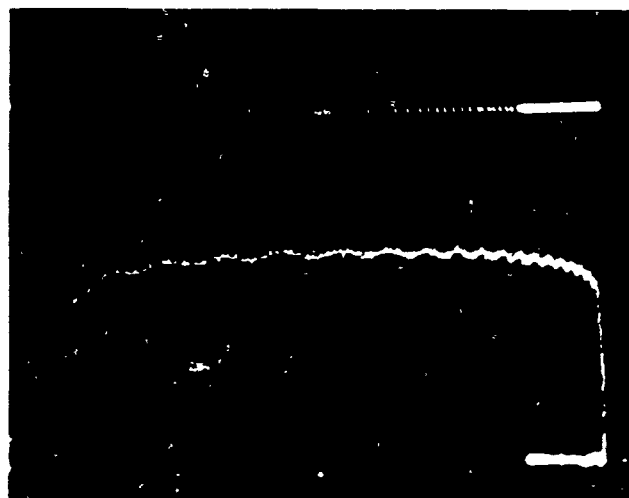


FIGURE 5. TYPICAL LOAD-STRAIN CURVE



FIGURE 6. ARCING CONDITION SHOWN BY 500°F TEST SPECIMEN

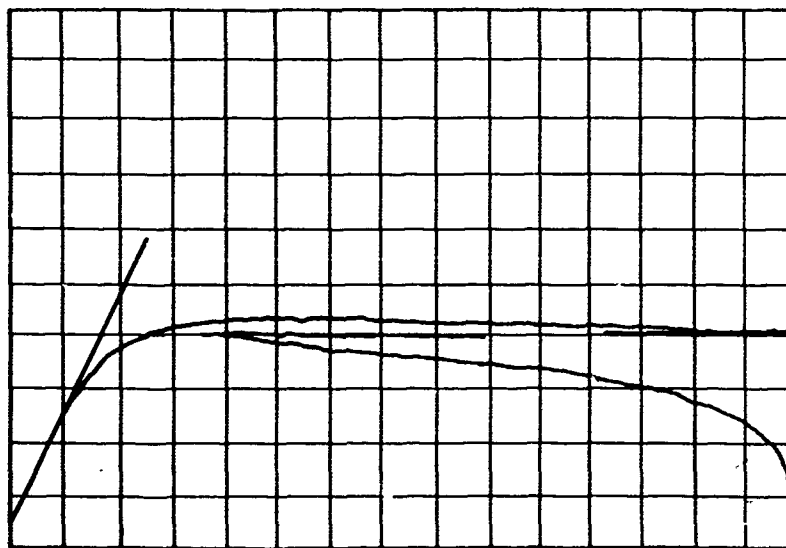


FIGURE 7. TYPICAL LOAD-STRAIN CURVE SHOWING UNIFORM ELONGATION DATA





FIGURE 8. TEMPERATURE GRADIENT CHECKOUT

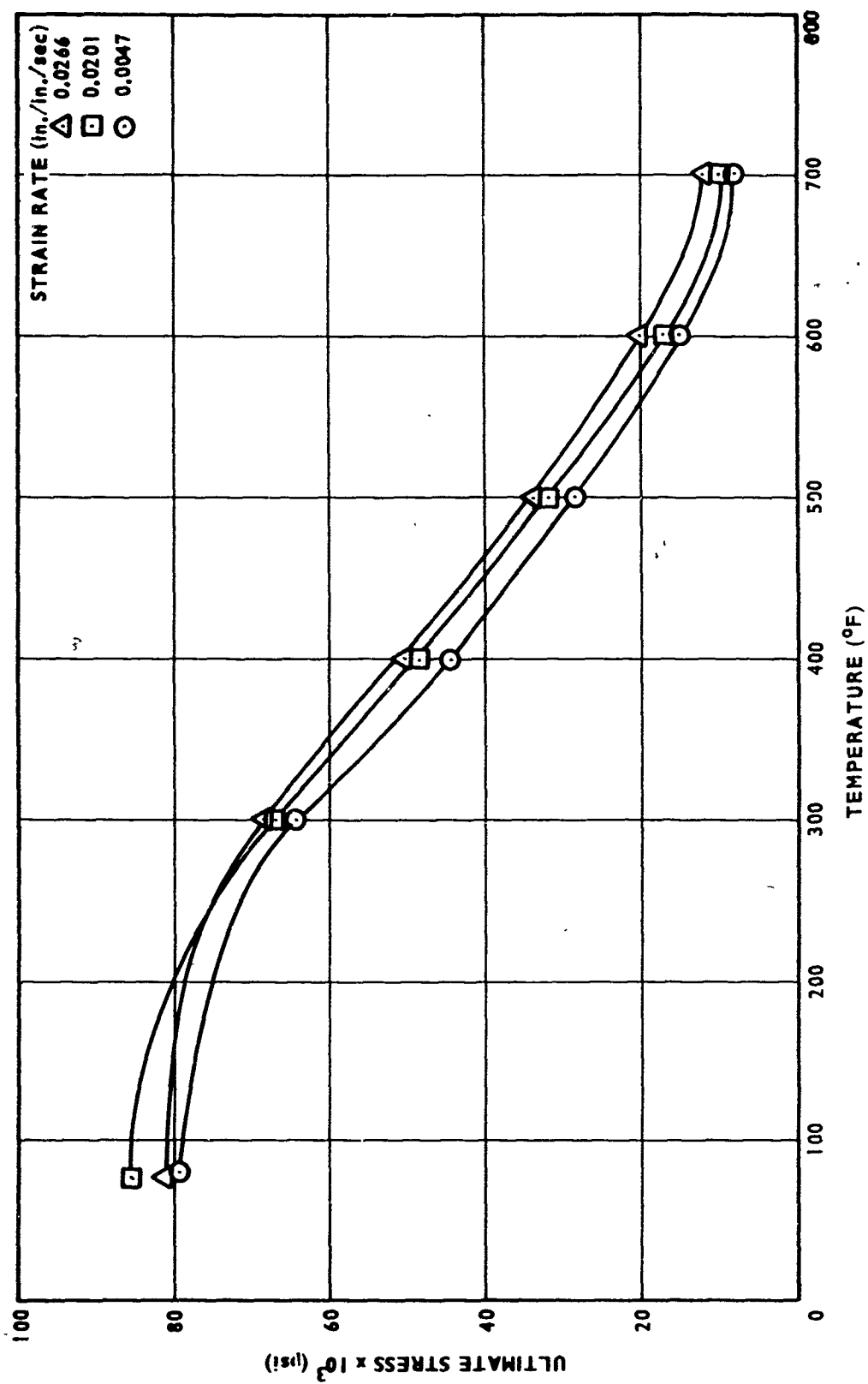


FIGURE 9. ULTIMATE STRESS-TEMPERATURE CURVES, LONGITUDINAL SPECIMEN

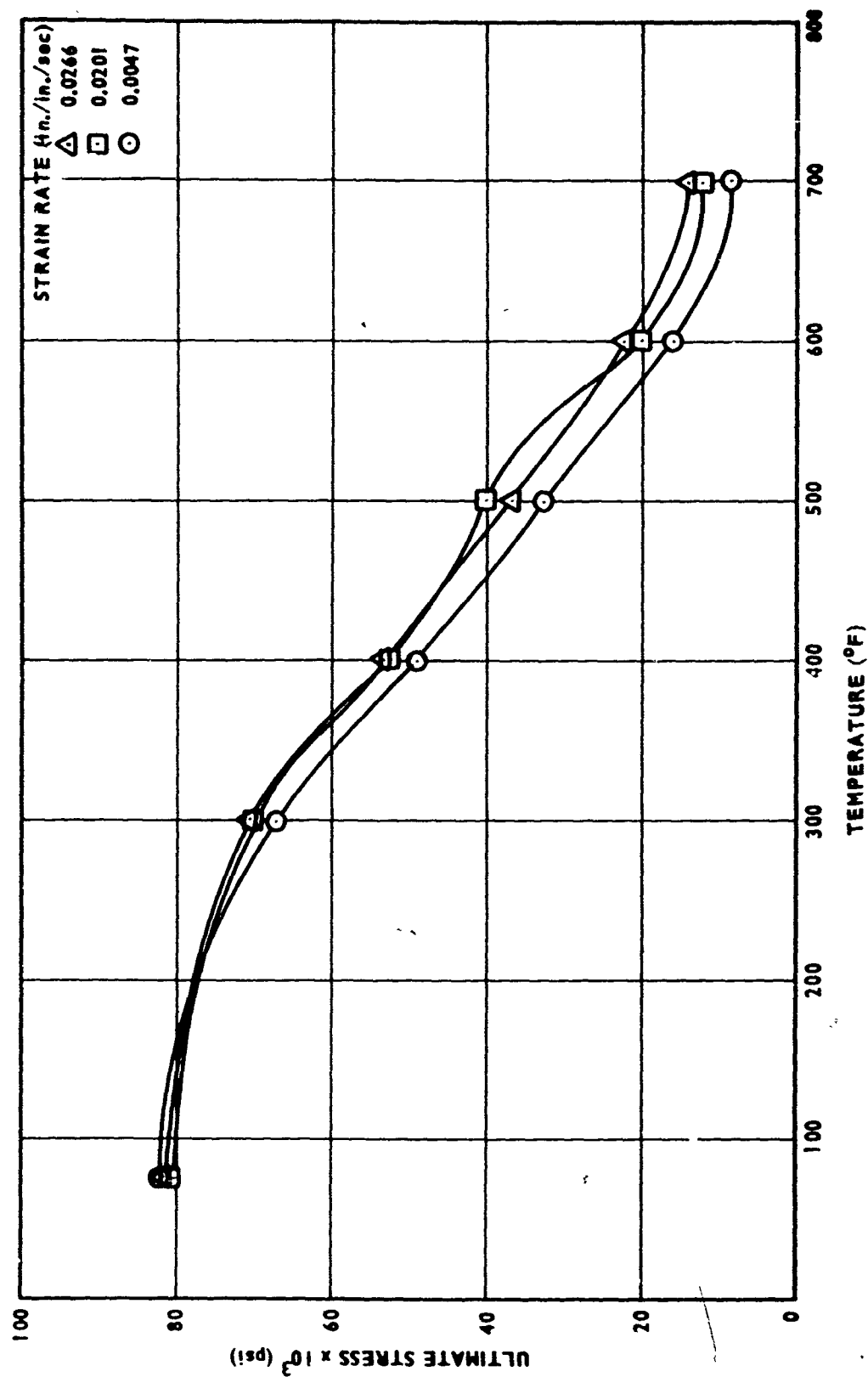


FIGURE 10. ULTIMATE STRESS-TEMPERATURE CURVES, TRANSVERSE SPECIMEN

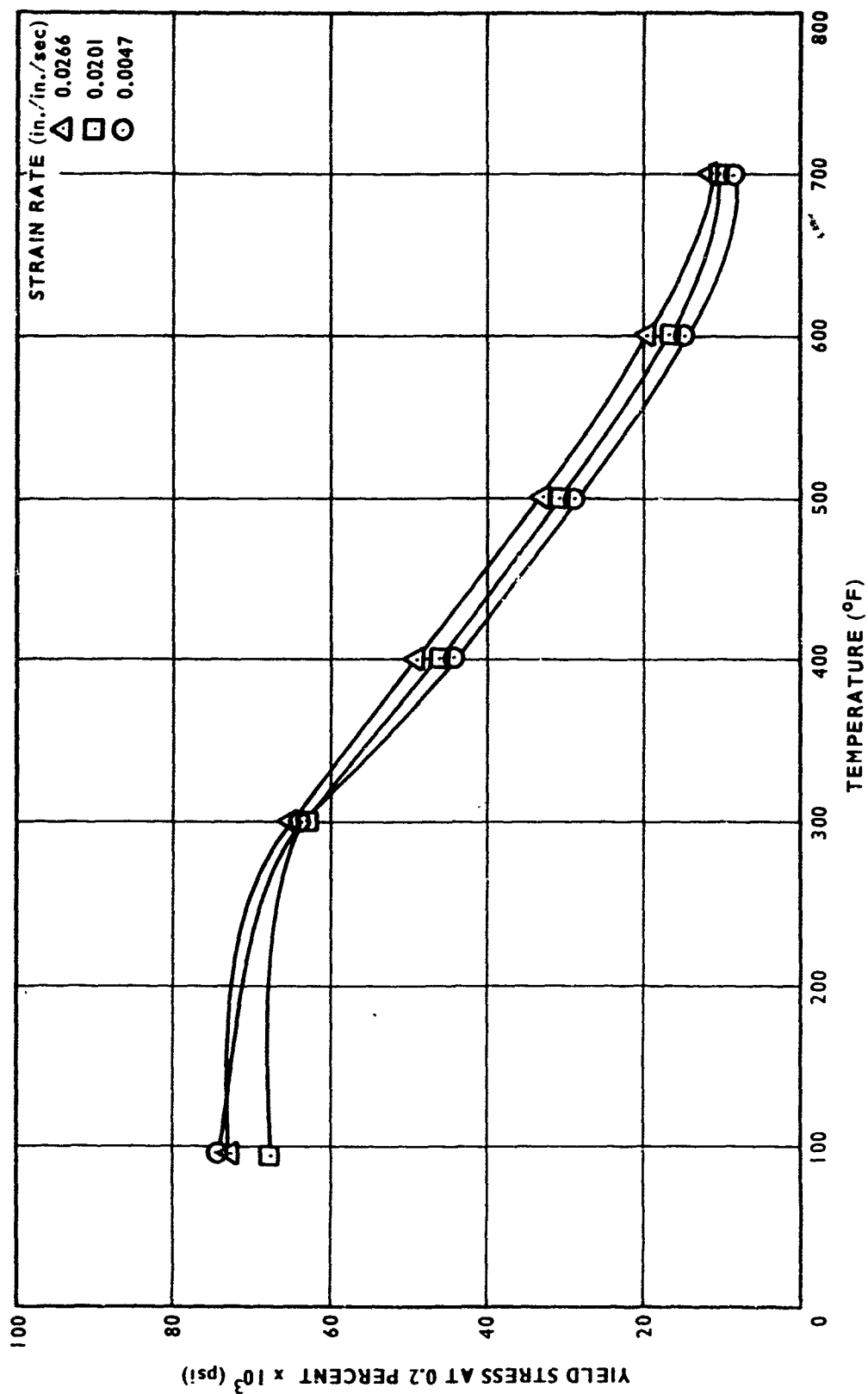


FIGURE 11. YIELD STRESS-TEMPERATURE CURVES, LONGITUDINAL SPECIMEN

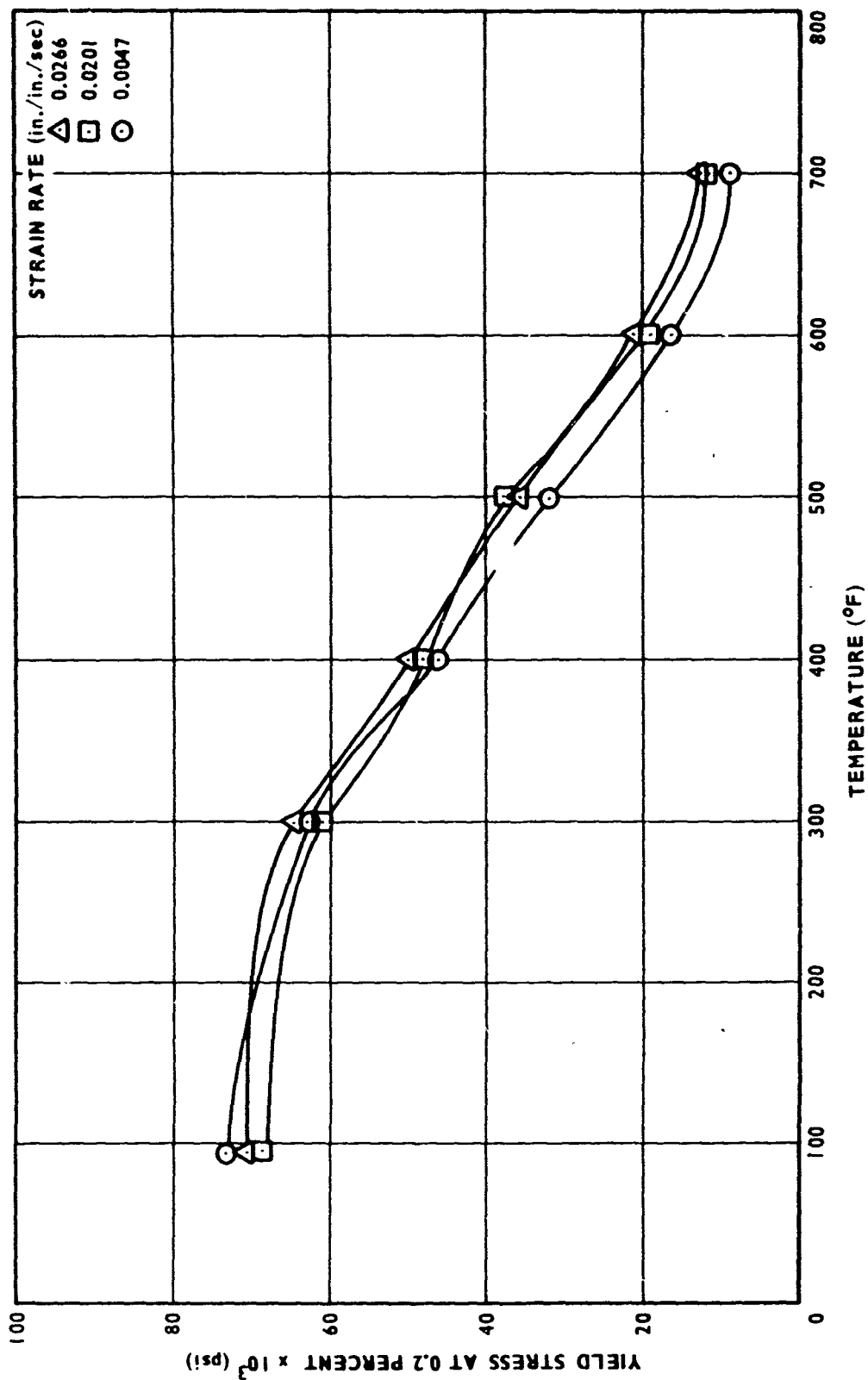


FIGURE 12. YIELD STRESS-TEMPERATURE CURVES, TRANSVERSE SPECIMEN

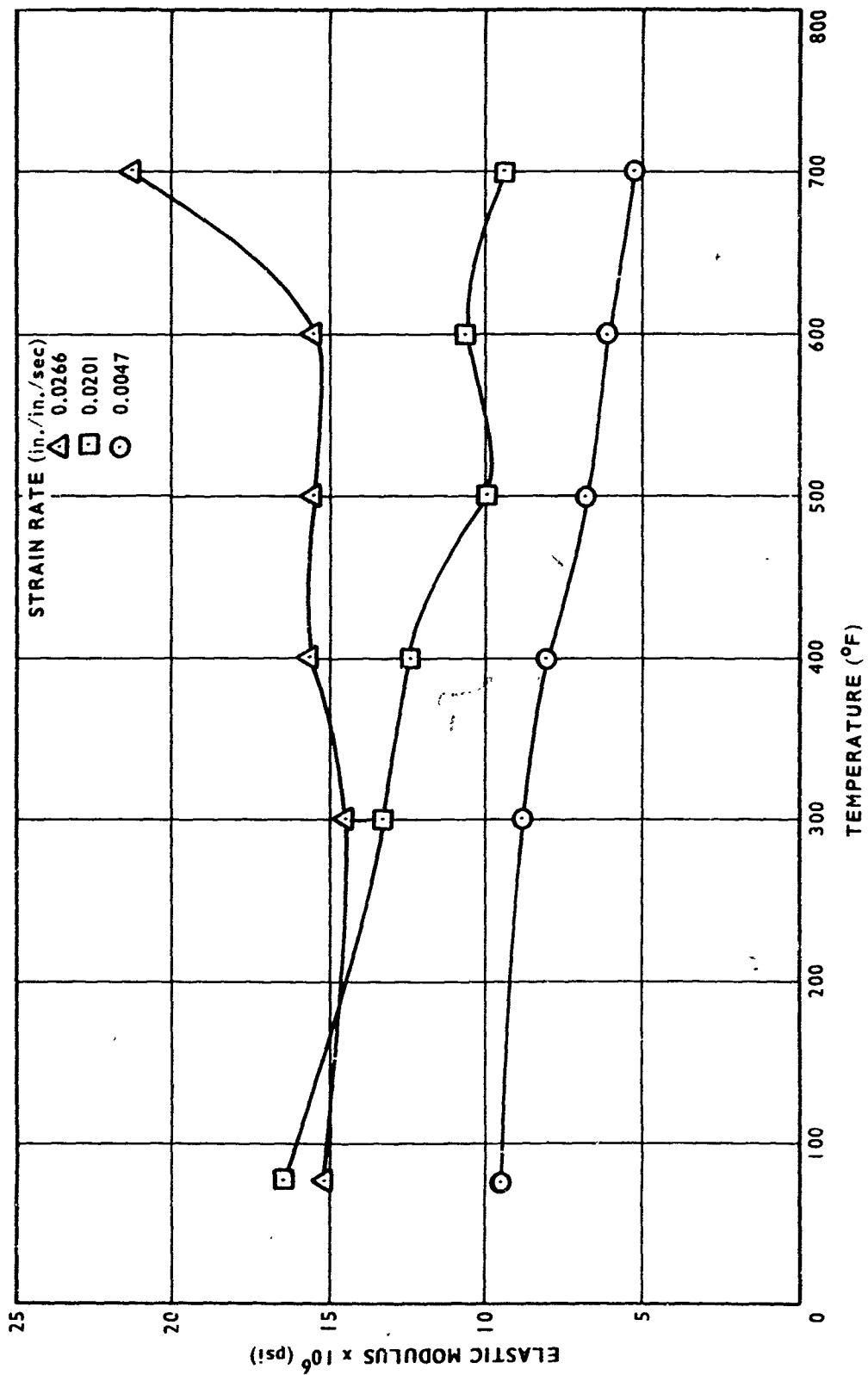


FIGURE 13. ELASTIC MODULUS-TEMPERATURE CURVES, LONGITUDINAL SPECIMEN

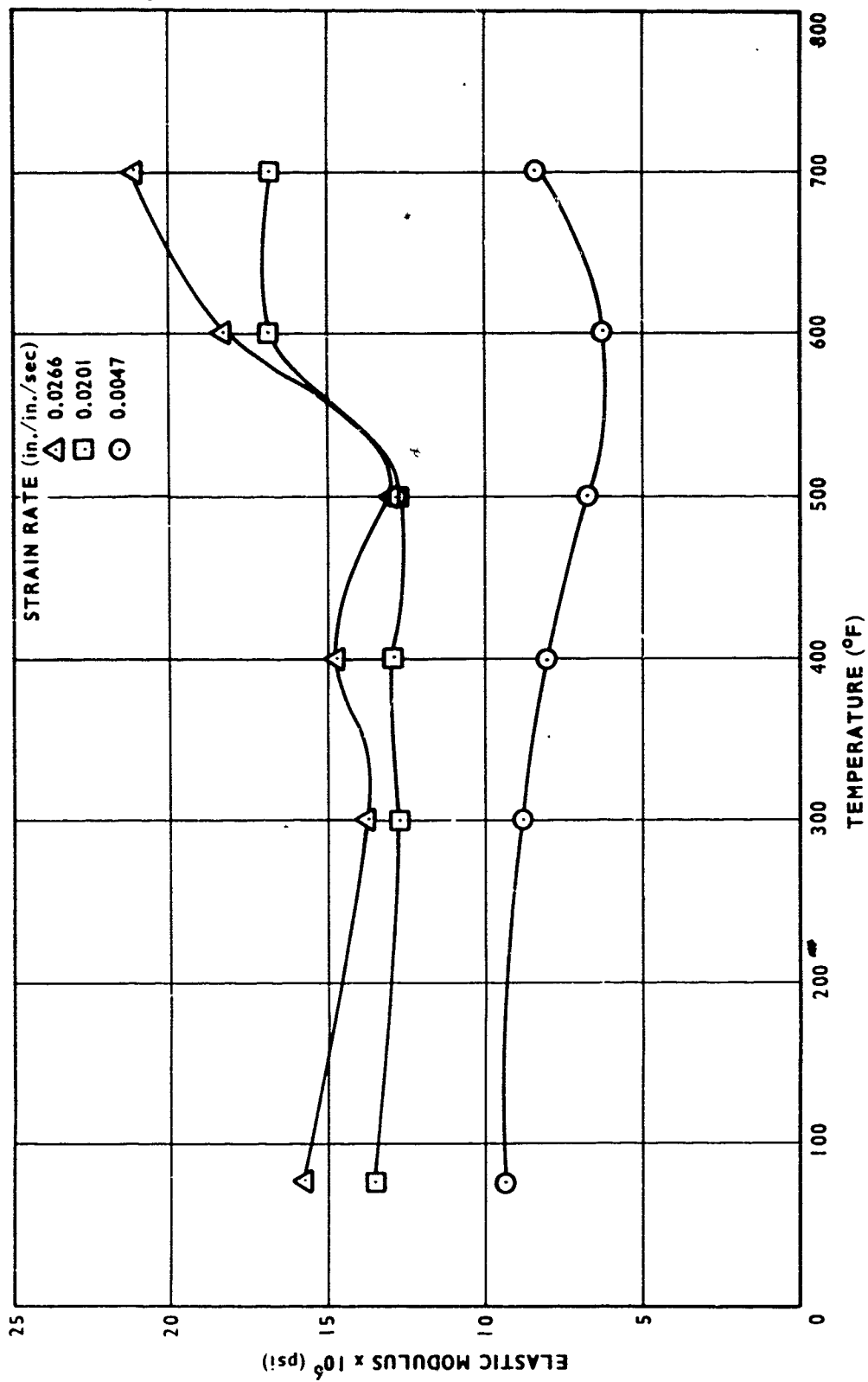


FIGURE 14. ELASTIC MODULUS-TEMPERATURE CURVES, TRANSVERSE SPECIMEN

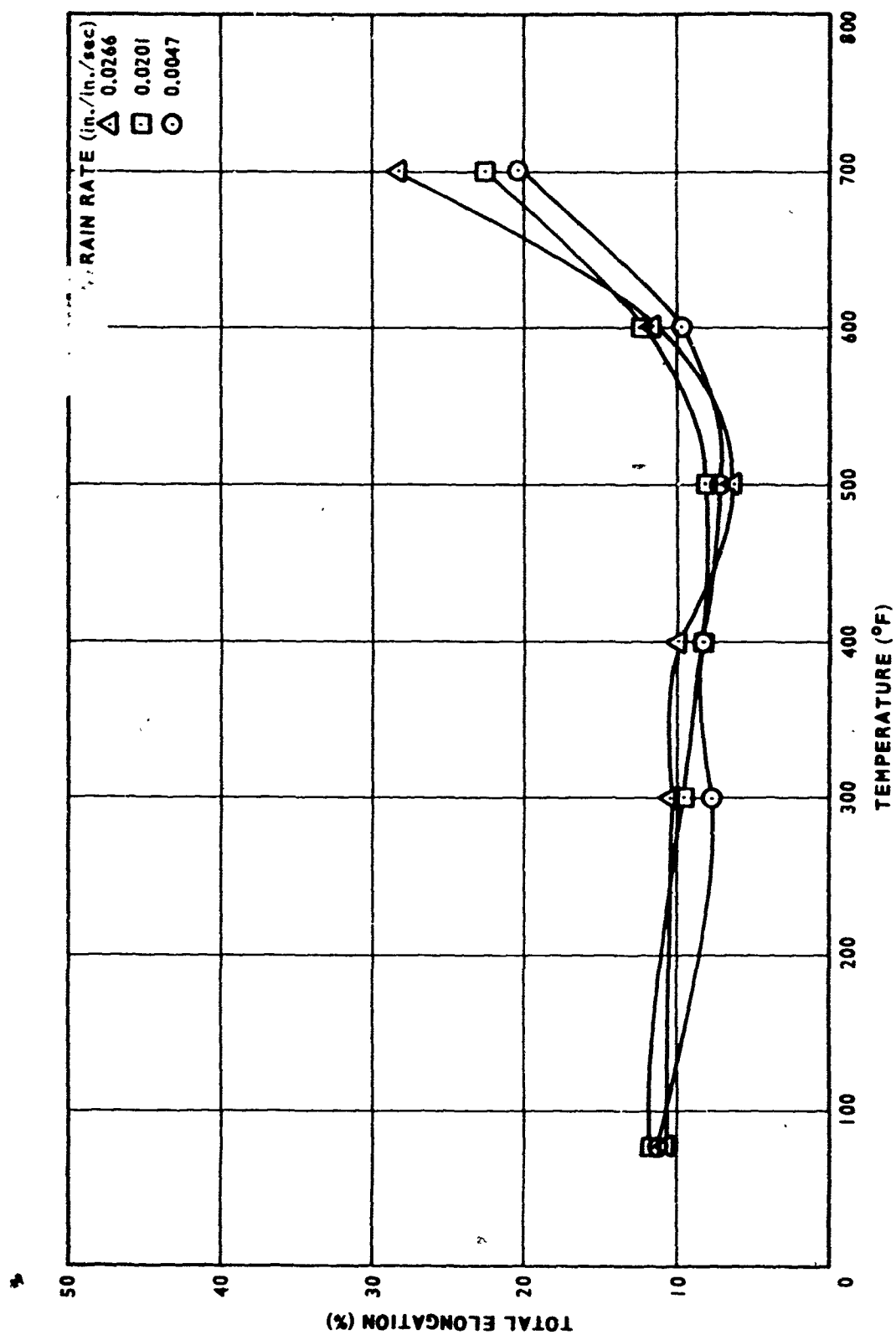


FIGURE 15. TOTAL ELONGATION-TEMPERATURE CURVES, LONGITUDINAL SPECIMEN



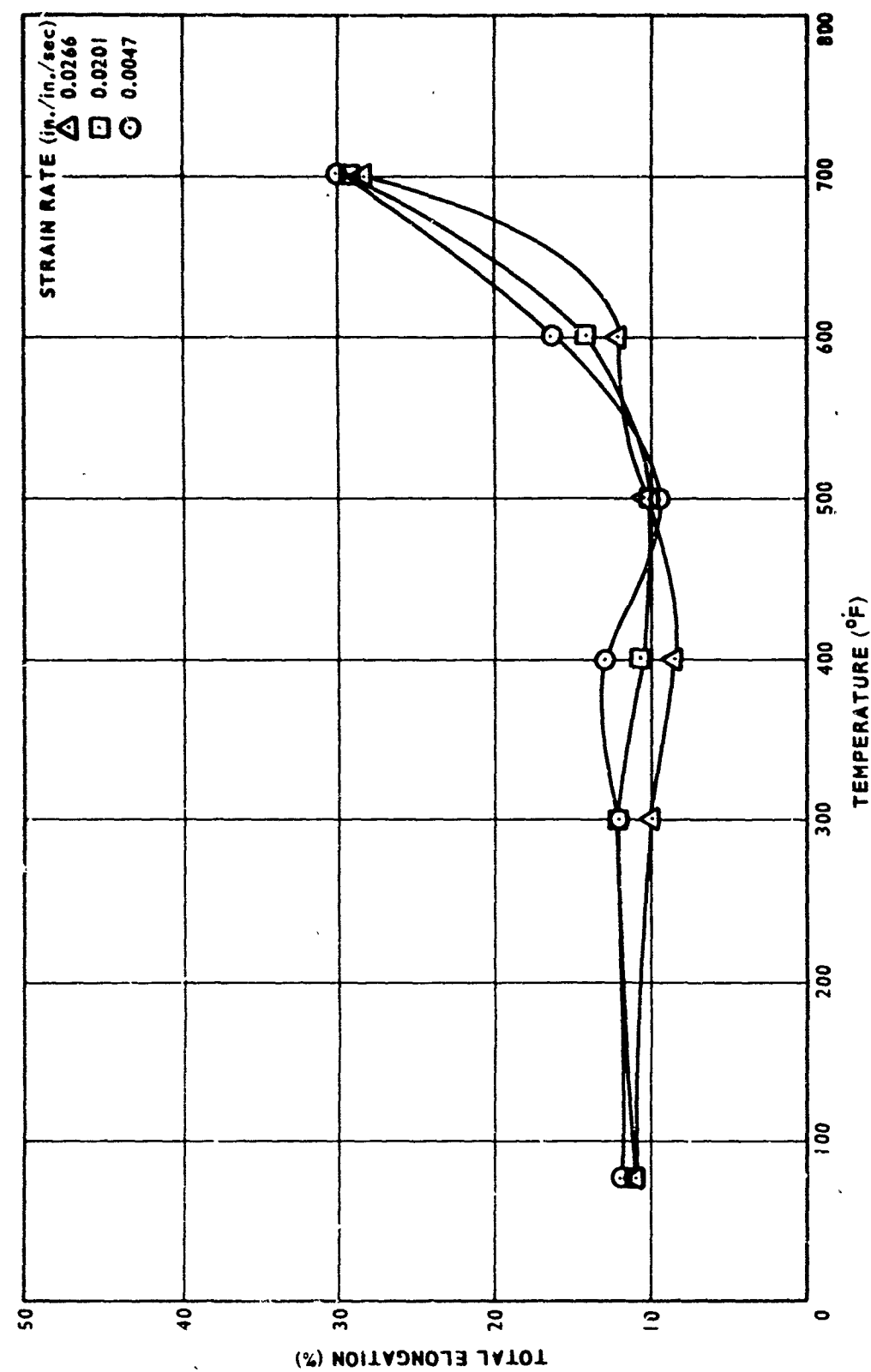


FIGURE 16. TOTAL ELONGATION-TEMPERATURE CURVES, TRANSVERSE SPECIMEN

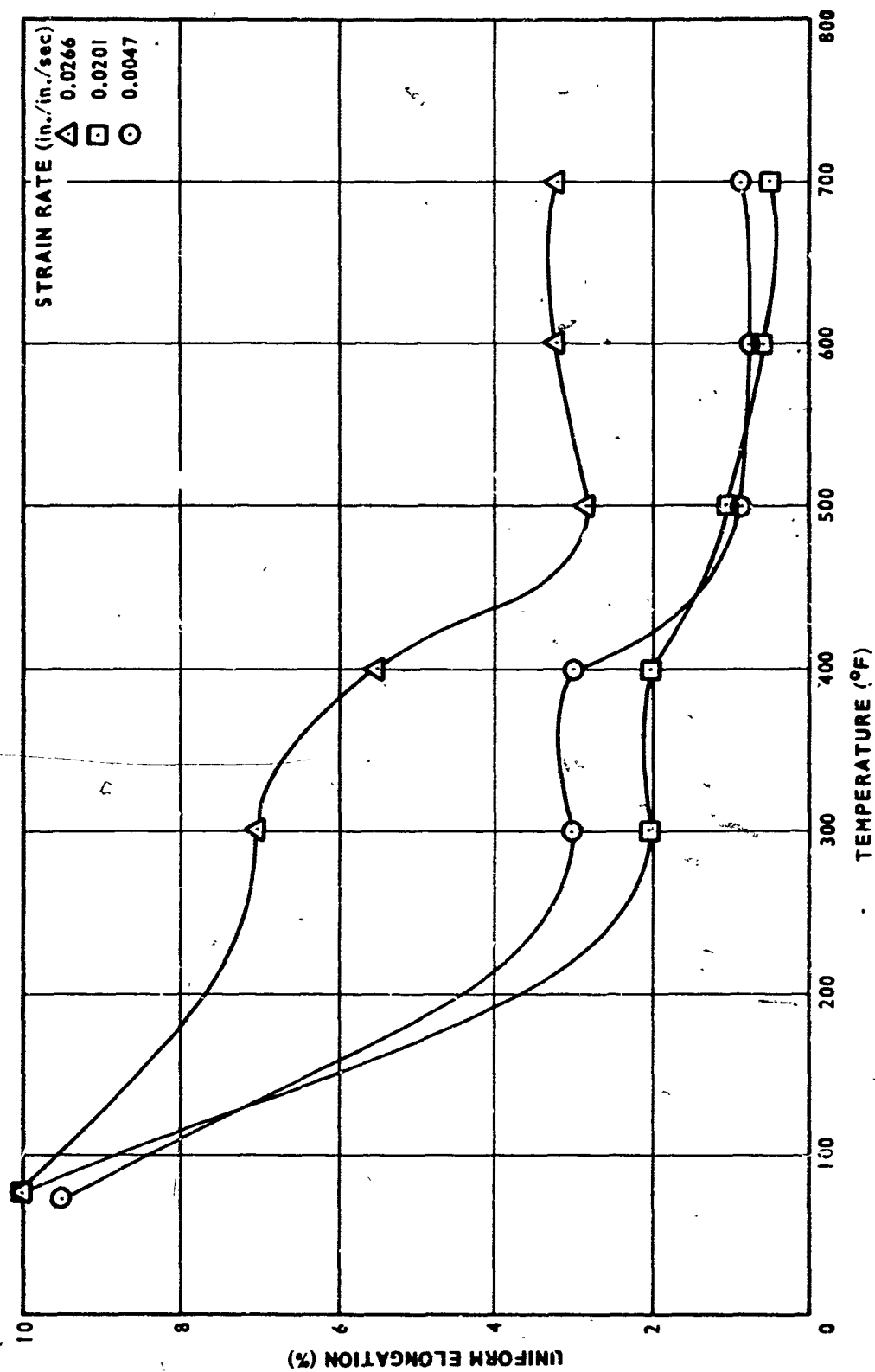


FIGURE 17. UNIFORM ELONGATION-TEMPERATURE CURVES, LONGITUDINAL SPECIMEN

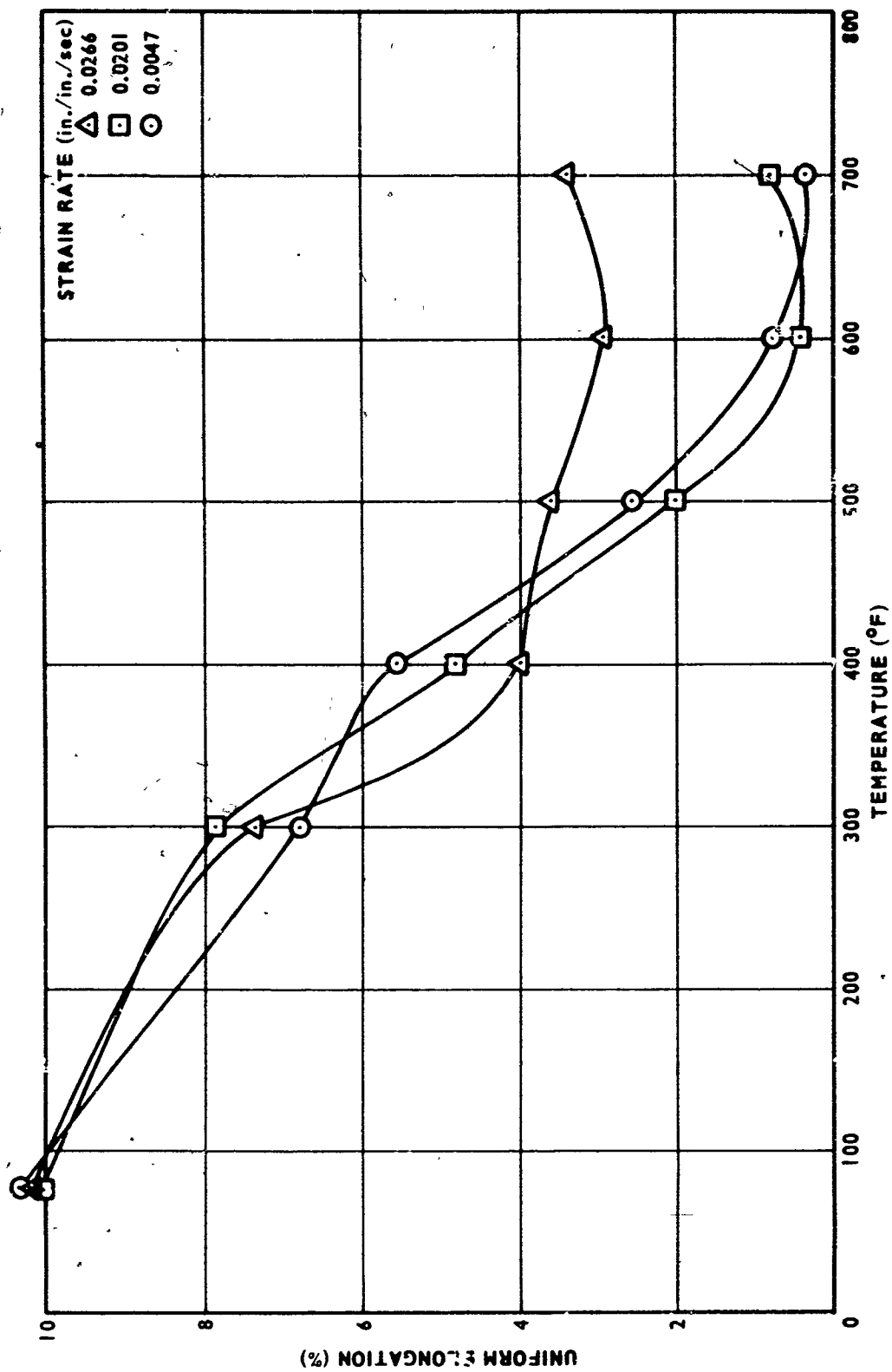


FIGURE 18. UNIFORM ELONGATION-TEMPERATURE CURVES, TRANSVERSE SPECIMEN

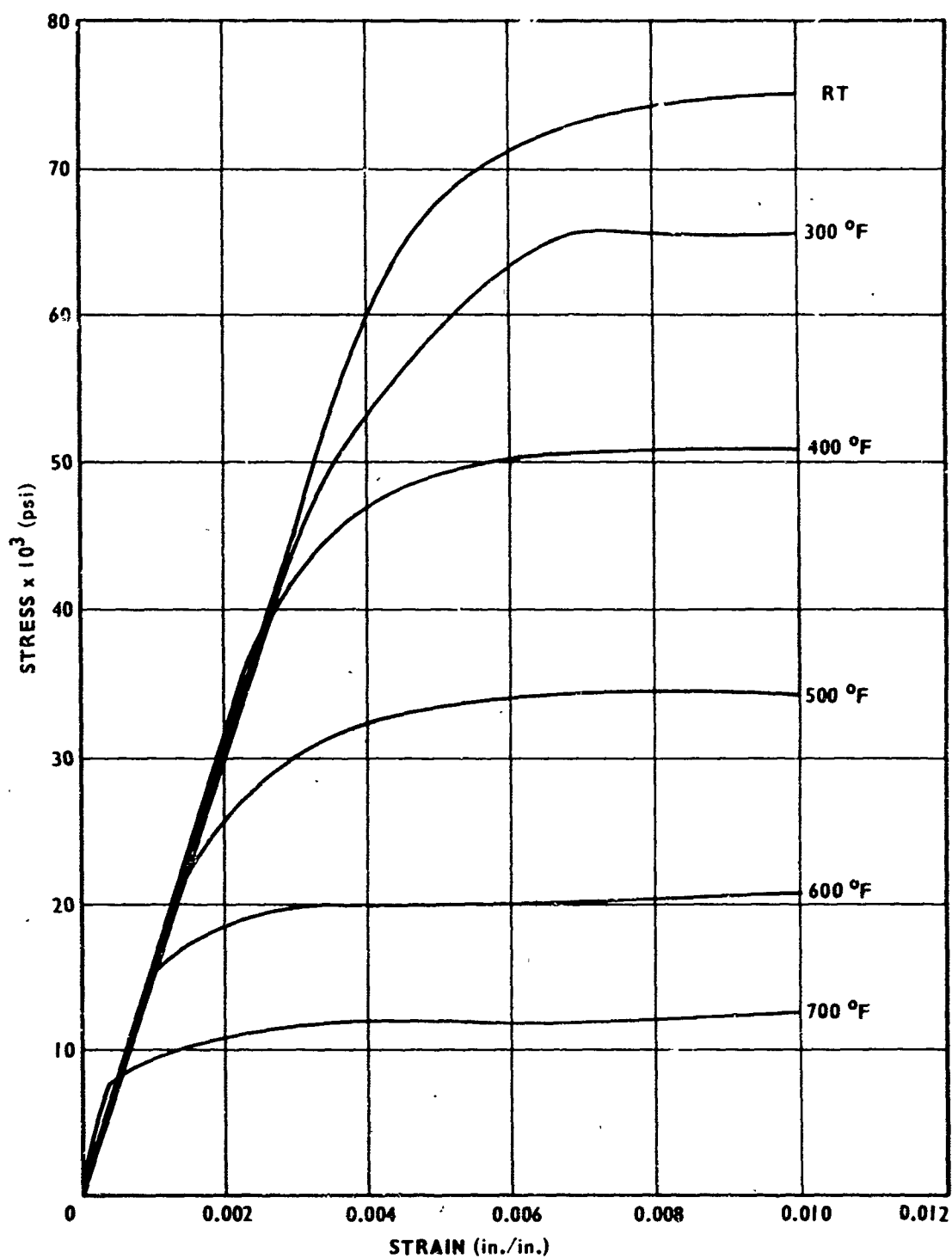


FIGURE 19. STRESS-STRAIN CURVES, LONGITUDINAL SPECIMEN,  
0.0266-in./in./sec STRAIN RATE

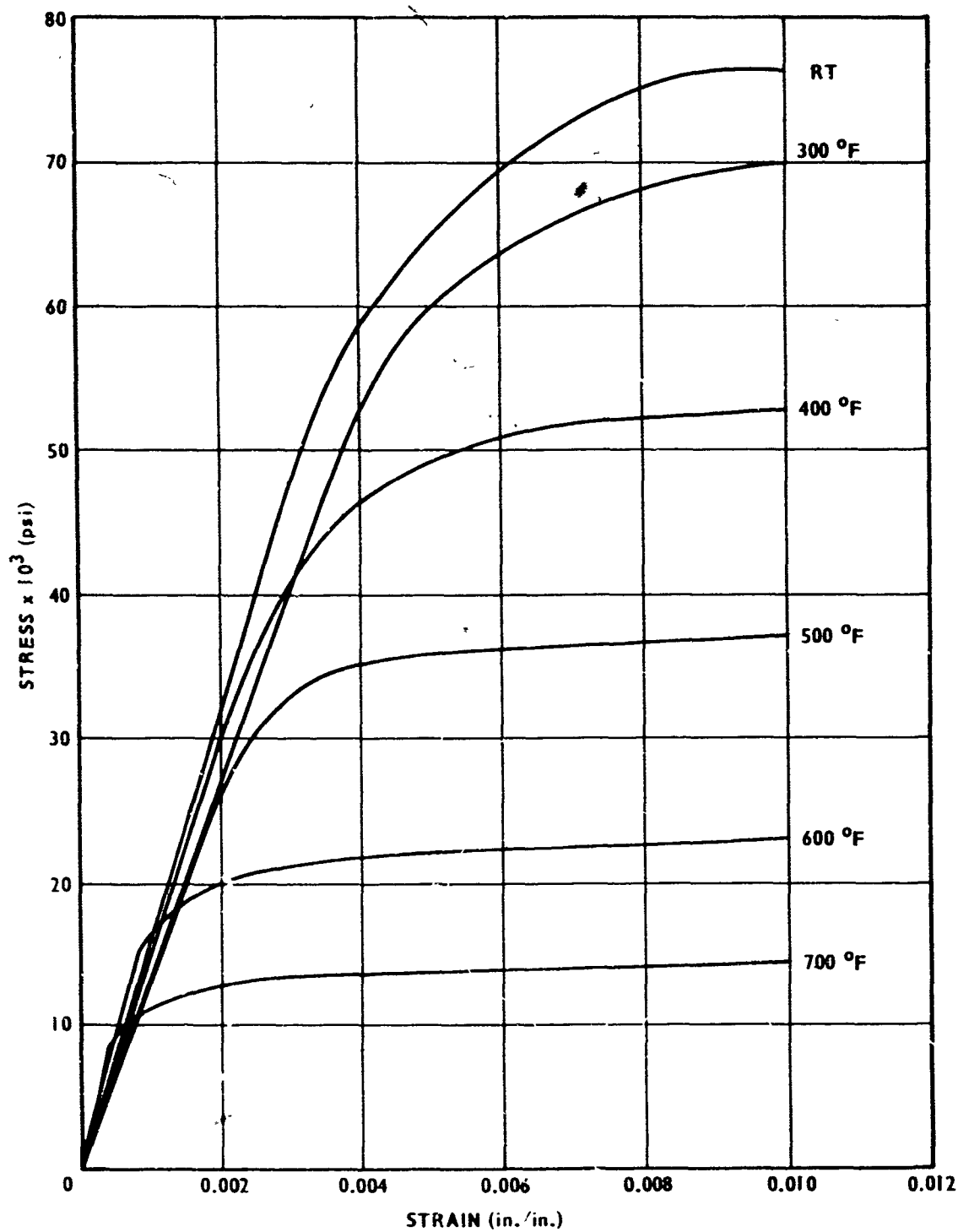


FIGURE 29. STRESS-STRAIN CURVES, TRANSVERSE SPECIMEN,  
0.0266-in./in./sec STRAIN RATE

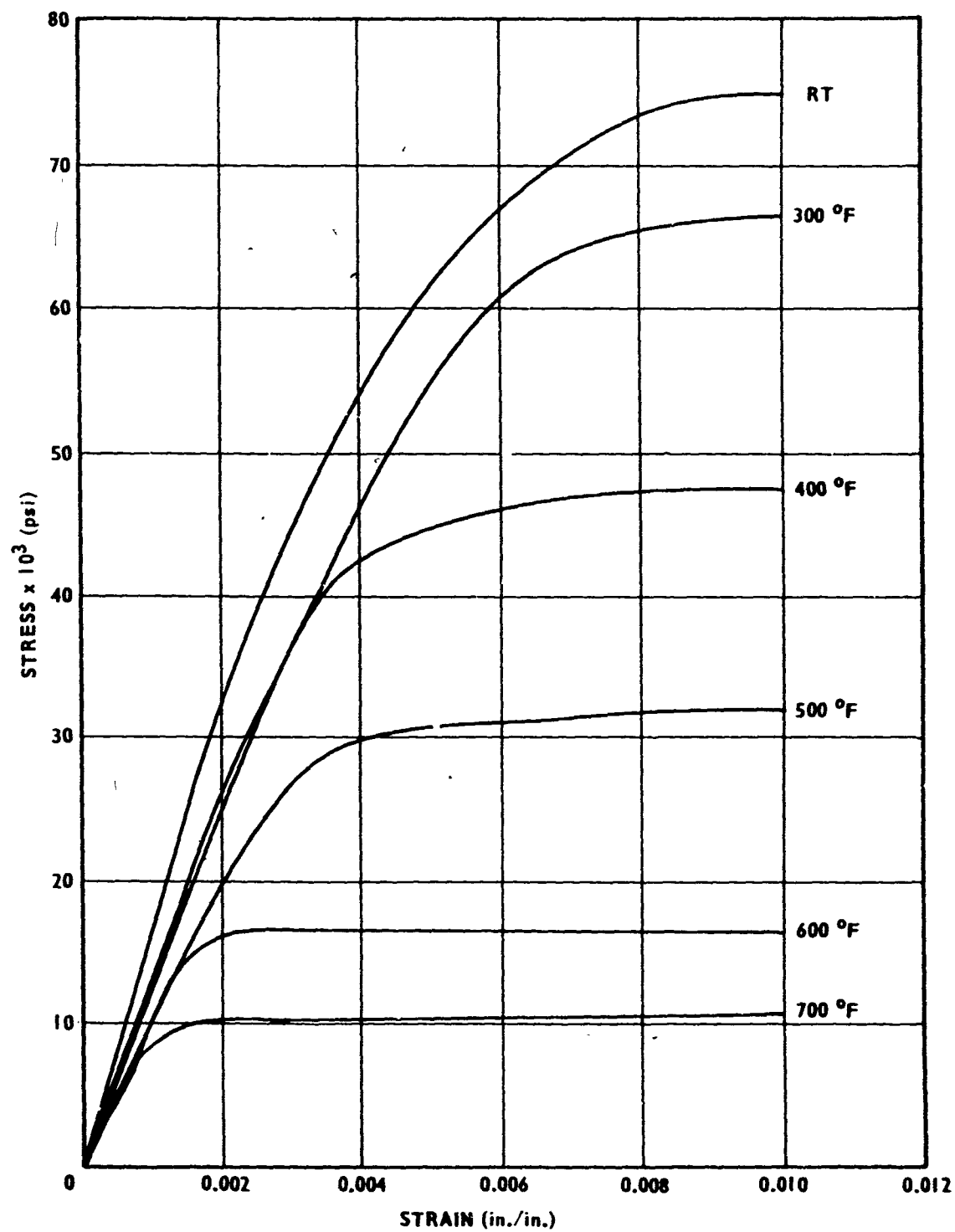


FIGURE 21. STRESS-STRAIN CURVES, LONGITUDINAL SPECIMEN,  
0.0201-in./in./sec STRAIN RATE

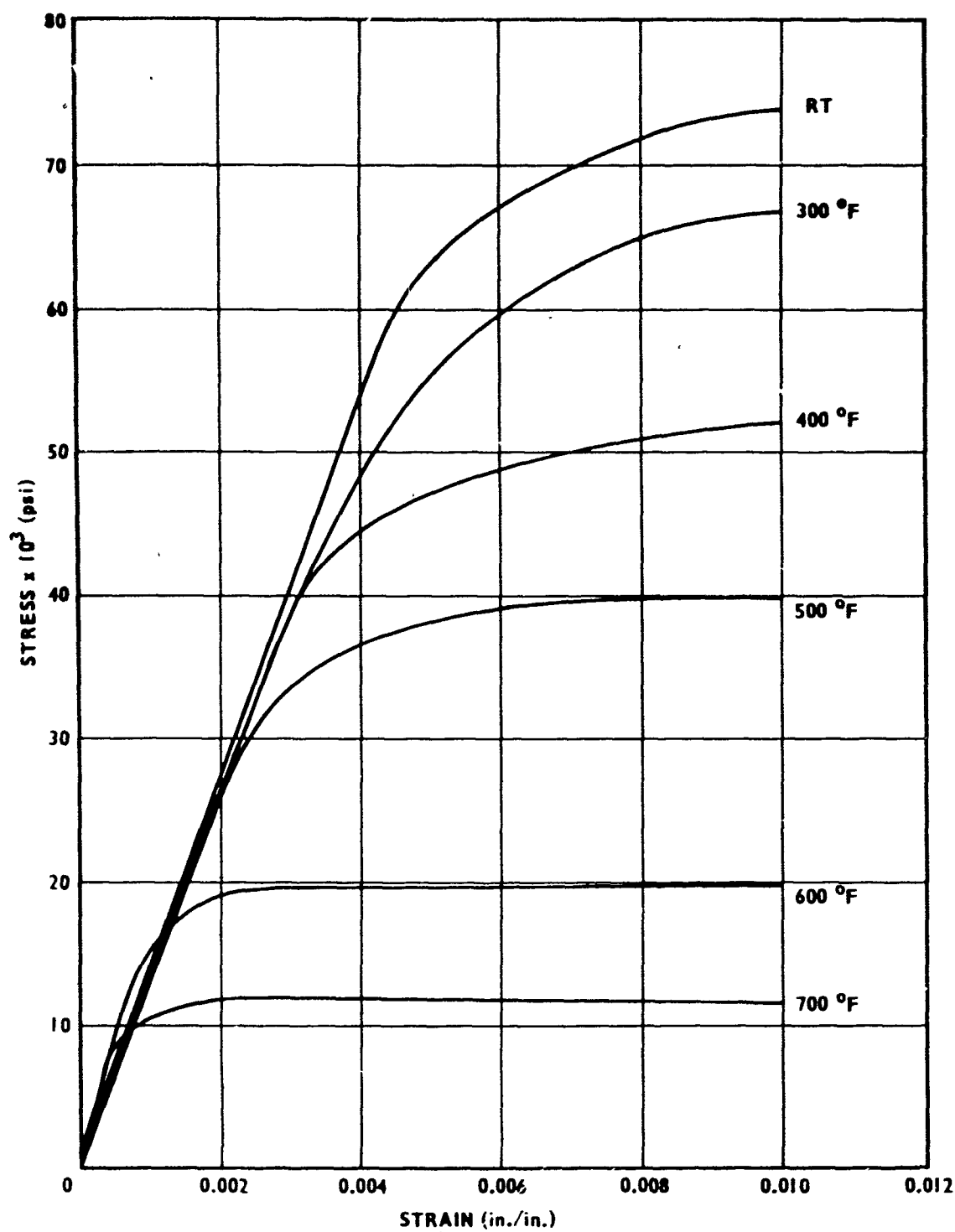


FIGURE 22. STRESS-STRAIN CURVES, TRANSVERSE SPECIMEN,  
0.0201-in./in./sec STRAIN RATE

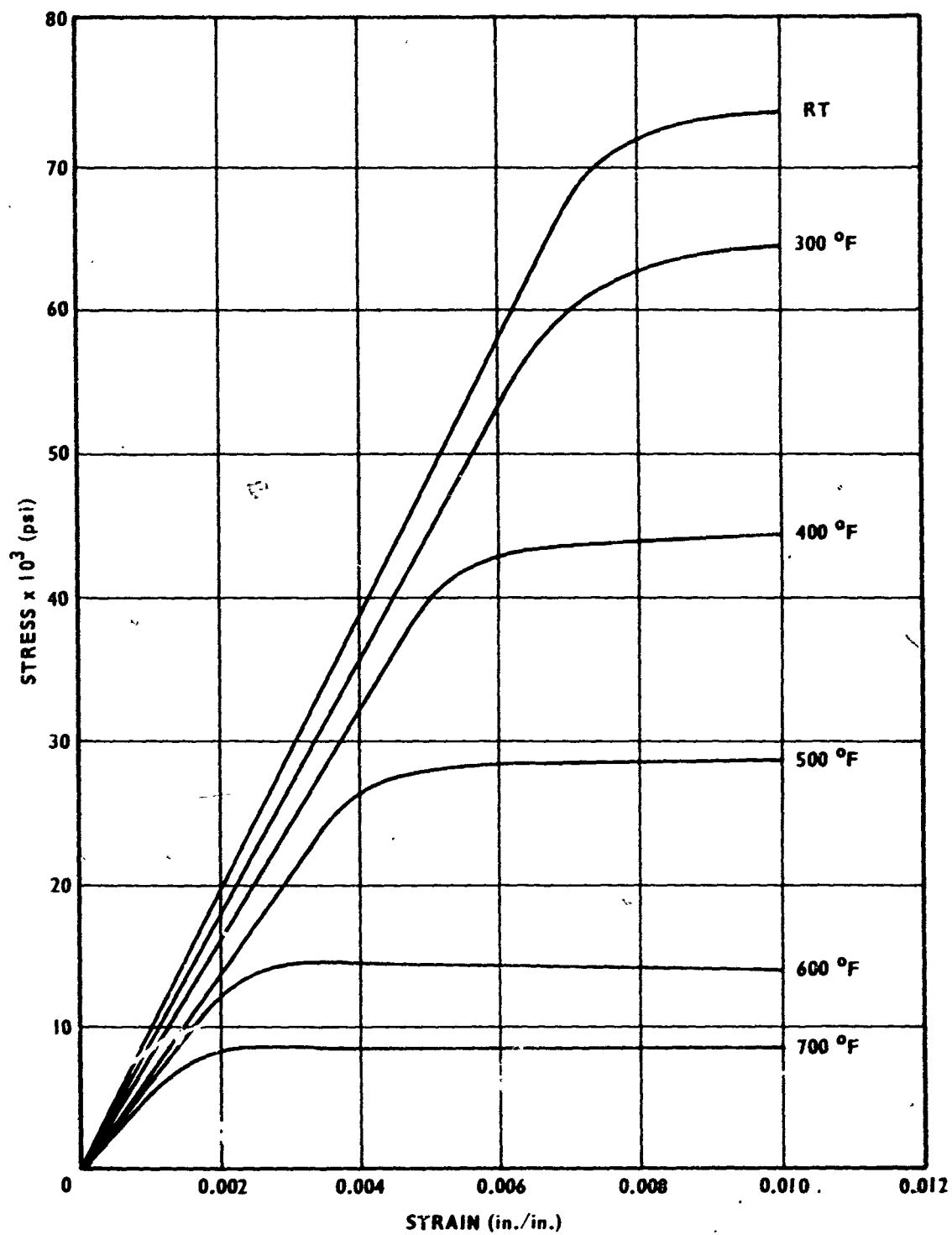


FIGURE 23. STRESS-STRAIN CURVES, LONGITUDINAL SPECIMEN,  
0.0047-in./in./sec STRAIN RATE



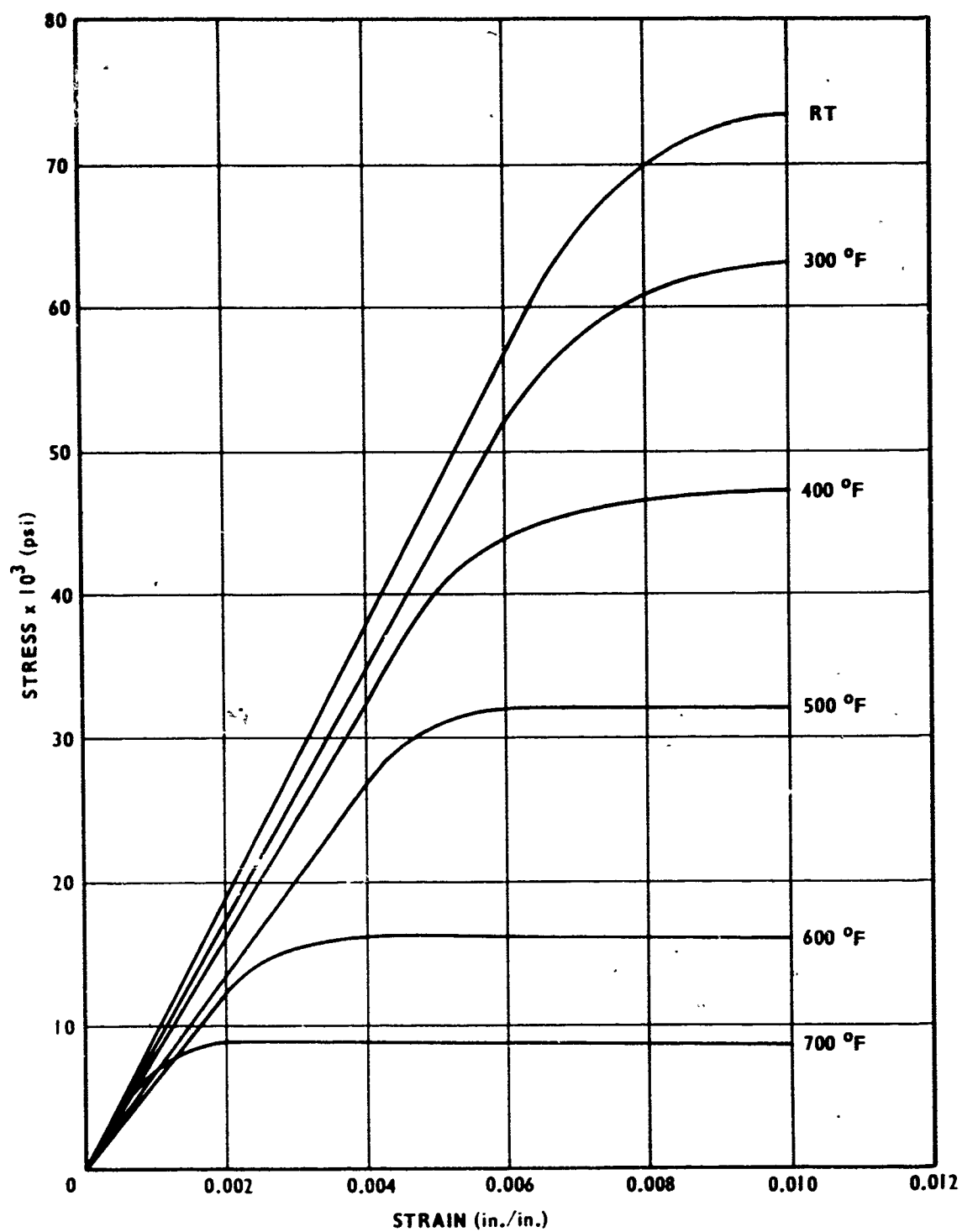


FIGURE 21. STRESS-STRAIN CURVES, TRANSVERSE SPECIMEN,  
0.0047-in./in./sec STRAIN RATE

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| 4. DESCRIPTIVE NOTES (Type of report and inclusive dates)<br>Technical Report  |                             |   |  |
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| 11. SUPPLEMENTARY NOTES<br>None  |                             | 12. SPONSORING MILITARY ACTIVITY<br>Same as No. 1                                 |  |
| 13. ABSTRACT<br>The purpose of this report is to make available to the design engineer tensile property data on 7075-T6 aluminum, in the longitudinal and transverse directions, under conditions of rapid heating and loading.<br>The tensile property data reported are: ultimate tensile stress, ultimate yield stress (at 0.2-percent offset), elastic modulus, percent total elongation, and percent uniform elongation. These tensile properties were determined at strain rates of 0.0047, 0.0201, and 0.0266 in./in./sec and at temperatures from room temperature (78°F) to 700°F at 100° intervals, excluding 100° and 200°F. The time required to reach test temperature was, in most cases, less than 10 seconds.<br>Primary consideration is given to ultimate tensile and yield properties. Other tensile property data reported are secondary and should be used for design criteria only after consideration has been given to the methods used for obtaining and reducing these data.<br>The strength properties of the test material increased with an increase in strain rate from 300°F to 700°F with one exception at 500°F on the transverse specimens. However, from room temperature to 300°F, the strength properties showed almost no change with respect to strain rate except for a point at room temperature on the longitudinal specimens. |                             |   |  |

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|---|--------|----|--------|----|--------|----|
|   | ROLE   | WT | ROLE   | WT | ROLE   | WT |
| 7075-T6 aluminum<br>Tensile property data<br>Rapid heating and loading<br>Tensile stress<br>Yield stress<br>Elastic modulus<br>Elongation |        |    |        |    |        |    |

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